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Abstract

Dual-polarization radar often detects columnar regions of enhanced differential reflectivity (Z_{DR}) extending vertically above the environmental 0 °C level. Indicative of supercooled liquid drops and wet ice particles lofted by strong updrafts, these Z_{DR} columns are increasingly understood to be of use in predicting extreme rainfall. With the aim of achieving practical application of Z_{DR} column measurements, this paper focuses on the relationship between the height of Z_{DR} columns and rainfall intensity near the ground.

All the data on Z_{DR} columns analyzed in this study was collected from weather radar stations in Japan. The height of each column and rainfall rates at low levels were analyzed using an automated algorithm. A regression analysis result reveals peak column height to be positively correlated with maximum rainfall rate near ground level, and that rainfall intensity on the ground is likely to exceed 50 mm h^{-1} when radar identifies a Z_{DR} column. Furthermore, extreme rainfall with an intensity of 180 mm h^{-1} or more is likely associated with a column over 3 km tall from the 0 °C level. These findings suggest that surveillance of Z_{DR} columns can contribute to the reliability of very short-range forecasts or nowcasts as well as assist with the issue of early warnings of extreme rainfall and flash floods.

28 **Keywords** extreme event; radar; Z_{DR} column; rainfall intensity; short-
29 range forecast

30 **1. Introduction**

31 Increasing global warming has resulted in greater frequency and inten-
32 sity of extreme precipitation events around the world, caused by increased
33 evaporation and atmospheric water-holding capacity attributed to higher
34 temperatures, as governed by the Clausius–Clapeyron (CC) relation (e.g.,
35 Min et al. 2011; Seneviratne et al. 2021). Numerous studies have been car-
36 ried out on the association between atmospheric temperature and heavy pre-
37 cipitation, some of which demonstrate that the frequency of short-duration
38 extremes may even exceed predictions based on the CC rate (e.g., Lenderink
39 and Van Meijgaard 2008) and that the intensity of sub-daily extremes in-
40 creases more rapidly than that of daily-scale events (e.g., Westra et al.
41 2014).

42 In recent decades, heavy precipitation events have often impacted human
43 society and the environment, mainly through rain-triggered disasters such
44 as floods, the most common natural hazard worldwide. Across the 2001 -
45 2020 period, an average of 357 annual catastrophic events were recorded, in
46 which floods (163) predominated (Centre for Research on the Epidemiology
47 of Disasters 2022b). In 2022, India and Pakistan experienced devastating

48 floods after extreme rainfall, each with more than one thousand deaths
49 (Centre for Research on the Epidemiology of Disasters 2022a). Flood risks
50 such as these are predicted to increase with the acceleration of urbaniza-
51 tion, due to the expansion of impervious surfaces and subsequent loss of
52 infiltration capacity (e.g., Tingsanchali 2012).

53 The major damage that is often caused by extreme rainfall is prompt-
54 ing research on enhancing the resolution of operational numerical weather
55 prediction models to provide more realistic forecasts of local weather, espe-
56 cially of precipitation. Despite the increasing accuracy of rainfall forecasts,
57 an element of uncertainty remains in all models. A large proportion of
58 this uncertainty derives from assumptions made in the parameterization of
59 unresolved cloud microphysical processes. However, a certain amount of
60 information can be gained from dual-polarization radar observations (e.g.,
61 Roberts and Lean 2008; Seifert 2011; Adachi et al. 2015; Trömel et al.
62 2021).

63 The National Weather Service (NWS) completed the dual-polarization
64 upgrade of its Weather Service radar (WSR-88D) in 2013 (Gerard 2021), and
65 the Japan Meteorological Agency (JMA) started upgrading its operational
66 weather radar in March 2020 (Japan Meteorological Agency 2022). Sending
67 and receiving signals with both horizontal and vertical polarization, dual-
68 polarization radar, or polarimetric radar can provide beneficial polarimetric

69 variables that deliver information concerning hydrometeor size, shape, and
70 orientation by comparing the amplitudes and phases of the signals returned
71 at both polarizations. Of these variables, the differential reflectivity, or
72 Z_{DR} , is a function of the shapes of hydrometeors. Higher values of Z_{DR} are
73 recorded when raindrops grow and take on a more oblate spheroidal shape.

74 Polarimetric radar observations of deep convective clouds frequently
75 show upward extensions of positive Z_{DR} above the environmental 0 °C level
76 where ice particles are usually distributed. These signatures, known as
77 Z_{DR} columns, contain supercooled liquid drops lofted by strong updrafts
78 (Kumjian 2013b). Recent studies have shown that Z_{DR} column evolution is
79 linked to convective cloud development. For example, Kumjian et al. (2012)
80 clarified the correlation between Z_{DR} column height and updraft intensity
81 using a simplified theoretical model, and Adachi et al. (2013) presented
82 a method of detecting potentially hazardous convective clouds that pro-
83 duce extreme rainfall by identifying Z_{DR} columns. Picca et al. (2010) and
84 Kumjian et al. (2014) describe how growth in the horizontal and vertical
85 directions of Z_{DR} columns precedes, by 10 - 30 minutes, an increase in low-
86 level radar reflectivity. Snyder et al. (2015) proposed an automated Z_{DR}
87 column algorithm designed to monitor the changes in Z_{DR} column height
88 and provide near-real-time information on the intensity and location of up-
89 drafts. Kuster et al. (2020) state that Z_{DR} columns can be used to arrive

90 at specific warning decisions for convective storms.

91 Despite these findings, the relationship between Z_{DR} column height and
92 rainfall intensity produced by the convective cloud has hitherto not been
93 quantitatively evaluated. This prompted us to investigate the relationship
94 between peak Z_{DR} column height and momentary maximum rainfall rate
95 near ground level using regression analysis of the rapid-update radar data
96 observed in the Tokyo metropolitan area with a view to the more general
97 application of Z_{DR} column information to short-term rainfall prediction.

98 This paper focuses on isolated Z_{DR} columns producing localized heavy
99 rainfall for ease of analysis and looks at those measured by the dual-polarization
100 Doppler weather radar at Haneda airport (Haneda radar) on 11 July 2021.
101 The next section describes the instrumentation and analytical data. Section
102 3 covers data analysis techniques using dual-polarization radar measure-
103 ments. Section 4 provides the analysis results of the relationship between
104 Z_{DR} column height and rainfall intensity near the ground, followed by our
105 Discussion in Section 5. The paper closes with a brief conclusion in Section
106 6 that summarizes our findings.

2. Instrumentation and analytical data

2.1 Dual-polarization weather radar

Doppler Radar for Airport Weather (DRAW) has been installed at major airports in Japan to monitor weather conditions for the safe operation of aircraft. The data sources in this study are the Haneda radar for the most part, but also the Narita radar at Narita International Airport for 0 °C level estimation. Haneda and Narita airports both operate C-band dual-polarized radar that provides a suite of polarimetric variables including the reflectivity factors (Z_H, Z_V), differential reflectivity (Z_{DR}), total differential phase shift (Ψ_{DP}), specific differential phase (K_{DP}), and co-polar correlation coefficient (ρ_{HV}). Their data are collected up to a maximum range of 120 km with an azimuthal resolution of 0.7° and a radial resolution of 150 m. The volume scans are updated every five minutes and each scan comprises twelve plan-position indicator (PPI) scans at elevation angles of $0.7^\circ, 1.1^\circ, 1.5^\circ, 2.1^\circ, 2.8^\circ, 3.8^\circ, 5.1^\circ, 6.9^\circ, 9.2^\circ, 12.5^\circ, 17.0^\circ$, and 90° . Five PPI scans at an elevation angle of 0.7° are included in each volume scan to improve the time resolution near the ground. The details of the Haneda radar are given in Table 1.

Table 1

125 2.2 *Surface observations*

126 a. *Disdrometer*

127 The Parsivel is a laser-based optical disdrometer for simultaneous mea-
128 surement of PARTicle SIze and VELOCITY of hydrometeors, designed by
129 Löffler-Mang and Joss (2000) and formerly manufactured by PM Tech, but
130 by OTT after 2004. In this study, we employed an OTT Parsivel (Version
131 1) disdrometer installed at the Kumagaya observation site.

132 The Parsivel is equipped with a laser sensor that produces a horizontal
133 sheet of light measuring 30 mm \times 180 mm, with a transmitter and receiver
134 integrated into a single protective housing. Precipitation particles passing
135 through the laser beam block a portion of the beam in proportion to their
136 diameter, causing a reduction of the output voltage. The maximum atten-
137 uation of the signal is a measure of the particle size, and the time taken for
138 the particle to pass through the laser beam allows an estimate of its velocity
139 (e.g., Löffler-Mang and Joss 2000; OTT 2005).

140 The OTT Parsivel disdrometer can estimate particle sizes ranging from
141 0.2 mm to 25 mm in diameter and velocities from 0.2 m s⁻¹ to 20 m s⁻¹.
142 After determining their diameters and velocities, it classifies them into one
143 of 32 separate size and velocity classes with a high temporal resolution of
144 one minute. It is therefore more suitable than a tipping bucket rain gauge
145 for observations of heavy convective rainfall events of the type shown in this

146 study (Section 4.1).

147 *b. Surface observation network*

148 The Automated Meteorological Data Acquisition System (AMeDAS),
149 an observation network of Automatic Weather Stations (AWSs) run by the
150 JMA, measures precipitation, wind direction and speed, temperature, and
151 humidity to support real-time monitoring of weather conditions. The JMA
152 currently operates about 1,300 rain gauges at average intervals of 17 km
153 nationwide. Each gauge records the amount of precipitation in units of
154 0.5 mm with a temporal resolution of ten minutes (Japan Meteorological
155 Agency 2021). In this study, precipitation data obtained from the Kuma-
156 gaya observation site is used for accuracy verification of rainfall rates from
157 the co-located disdrometer.

158 *2.3 Case information*

159 The data analyzed in this study were collected using the abovementioned
160 instruments from 13:00 JST (Japan Standard Time: $\text{JST} = \text{UTC} + 9 \text{ h}$)
161 to 18:00 JST on 11 July 2021. On that day, dozens of Z_{DR} columns were
162 observed by the Haneda radar, and the atmospheric condition was unstable
163 due to a stationary front, resulting in heavy precipitation over the Kanto
164 region (eastern Japan). Figure 1 shows the distribution of the rainfall es-

165 timates and the locations of the instruments and the Tateno aerological
166 observation site (Section 3.1).

167 The findings from the quantitative data analysis are validated using the
168 data collected from 12:00 JST to 16:00 JST on 12 August 2020 (Section
169 5.5), when atmospheric instability caused by elevated ground temperatures
170 led to convective heavy precipitation over the Kanto region, coupled with
171 high atmospheric pressure across eastern and western regions of Japan.

Fig. 1

172 3. Data analysis techniques

173 To initiate the analysis, radar data expressed as radar-centered spheri-
174 cal coordinate were converted into geographic form as presented by Karney
175 (2011). Non-meteorological data with correlation coefficients (ρ_{HV}) of be-
176 low 0.8 and standard deviations of Ψ_{DP} exceeding 4° were removed (e.g.,
177 Ryzhkov and Zrnic 1998). Subsequently, the Z_{DR} biases introduced in the
178 radar hardware were corrected through regression analysis between Z_H and
179 Z_V using radar measurements at vertical incidence in light rain (e.g., Bringi
180 and Chandrasekar 2001). The reduction factors given by Teschl et al. (2008)
181 were employed to calibrate the effect of elevation angles on both Z_{DR} and
182 K_{DP} . Using the elevation-corrected K_{DP} , Z_H and Z_{DR} were corrected for
183 their attenuation as described in Bringi and Chandrasekar (2001).

184 *3.1 Z_{DR} column height*

185 Z_{DR} columns are identified as regions of high Z_{DR} extending above the
186 environmental 0 °C level, the height criterion. Since the signature of a
187 melting layer, known as the “bright band,” is more evident in ρ_{HV} fields
188 than in Z_H fields (e.g., Kumjian 2013b), vertical distributions of ρ_{HV} were
189 utilized to estimate the 0 °C level in this study. On the basis of the model
190 profile of ρ_{HV} adopted by Brandes and Ikeda (2004), we estimated the 0 °C
191 level at the top of the bright-band signature, assuming the 0 °C level to be
192 constant over the Kanto region while the data were collected. Unlike other
193 analyses, the data here were acquired by the Narita radar around 17:30 JST
194 when the signature appeared most clearly, not by the Haneda radar because
195 the signature was too obscure to estimate the 0 °C level. Figure 2 shows an
196 example of the distribution maps, in which the vertical axis represents the
197 height above ground level (AGL). The estimated 0 °C level approximately
198 corresponds to the results of aerological observations at the Tateno site,
199 located about 60 km northeast of the Haneda radar.

Fig. 2

200 Given that vertical resolutions become coarser with increasing elevation
201 angle, we adopted a fixed 3-dB threshold to define the periphery of the Z_{DR}
202 columns to obtain a more accurate estimation in preference to the 1- or 2-dB
203 threshold often used in other studies (e.g., Kumjian et al. 2014; Snyder et al.
204 2015). Accordingly, in this study, the Z_{DR} column height is the maximum

205 height of the 3-dB Z_{DR} contour from the 0 °C level. Each column height
206 in the time series was estimated by interpolating data along the movement
207 direction of the center, determined from the PPI scan data, with a width of
208 1 km (see Fig. 3a for a sample column, called “Column A” hereinafter) and
209 averaging the vertical locations of n points that are selected in descending
210 order from the highest one on the periphery, given that n grid cells exist
211 within 1 km along the horizontal axis. Here, the advective velocity of a cloud
212 is not taken into account because column height is immune to horizontal
213 cloud motion. The central axis of each column was also determined by
214 averaging the horizontal locations of the highest n points on the periphery.
215 Ultimately, the column height and the central axis at the time when column
216 height reached a peak were ascertained, along with the observation time.
217 An example of the estimated height and central axis of Column A is shown
218 in Fig. 3b. Note that the differential reflectivity Z_{DR} is linearly interpolated
219 in the figure.

Fig. 3

220 3.2 *Radar rainfall estimation*

221 A wide variety of physical and empirical approaches are generally taken
222 to estimate rainfall rates from polarimetric radar variables. In one of these
223 methods, Cifelli et al. (2011) describe an algorithm called CSU-ICE, which
224 discriminates between pure rain and mixed precipitation using the precip-

225 itation ice fraction in a radar volume. The ice fraction is estimated using
 226 the difference reflectivity Z_{DP} , defined as

$$Z_{\text{DP}} = 10 \log_{10} (Z_{\text{H}} - Z_{\text{V}}), \quad (1)$$

227 where Z_{H} and Z_{V} are linear scale values. However, Z_{DP} may be inaccurate
 228 in widespread heavy rain events such as those analyzed in this study due to
 229 the attenuation effects of Z_{H} and Z_{V} in the C-band. We therefore applied
 230 the CSU-ICE algorithm for mixed precipitation using $R(K_{\text{DP}})$ and $R(Z_{\text{H}})$
 231 to all samples. This algorithm is the same as that which JMA currently
 232 employs, expressed as

$$R(K_{\text{DP}}, Z_{\text{H}}) = \begin{cases} R(K_{\text{DP}}) = 129 \left(\frac{K_{\text{DP}}}{f} \right)^{0.85} & \text{if } K_{\text{DP}} > 0.6 \text{ deg/km and } Z_{\text{H}} > 38 \text{ dBZ;} \\ R(Z_{\text{H}}) = \left(0.005 \times 10^{\frac{Z_{\text{H}}}{10}} \right)^{\frac{1}{1.6}} & \text{otherwise,} \end{cases} \quad (2)$$

233 where R is rainfall rate in mm h^{-1} and f is a radar frequency in GHz (Bringi
 234 and Chandrasekar 2001). Note that Z_{H} here is not a rain-only reflectivity
 235 but a version observed and corrected.

236 $R(K_{\text{DP}})$ is commonly exploited because of its high accuracy when used
 237 for heavy rainfall estimation, since K_{DP} has the advantage of being immune
 238 to attenuation and is less dependent on the variation of drop size distribu-
 239 tion (DSD). In contrast, its low accuracy in light rain results from the fact
 240 that K_{DP} is not sensitive to spherical particles, and its signal falls below the
 241 background noise level (e.g., Sachidananda and Zrnica 1986). Therefore, a

242 traditional $Z - R$ relation, or $R(Z_H)$, applies with low K_{DP} and/or reflectiv-
243 ity, mostly in light rain after Z_H being corrected. Based on the assumption
244 of Marshall-Palmer DSD (Marshall and Palmer 1948), $R(Z_H)$ is strongly af-
245 fected by variability of precipitation type (e.g., Bennartz and Petty 2001).
246 Taking into account the uncertainties inherent in DSD parameterization,
247 we additionally calibrated Z_H by minimizing discrepancies in rainfall rates
248 between Z_H -derived estimates and the disdrometer measurements described
249 in the Appendix.

250 3.3 *Low-level maximum rainfall rate*

251 The maximum rainfall rate near ground level associated with each col-
252 umn was estimated from the data observed at the lowest elevation angle of
253 0.7° by the Haneda radar. Although radar data at this angle are subject to
254 beam blockage due to ground clutter in certain directions, as shown in Fig.
255 4, the highest temporal resolution of one minute is necessary for analyzing
256 the time series of convective rainfall. Each maximum rainfall rate in the
257 time series was estimated by

- 258 1. extracting rainfall rates in a rectangular area measuring $10 \text{ km} \times 30$
259 km between 5 km to windward and 25 km to leeward from the central
260 axis at the time when column height reached a peak, based on wind
261 speed and direction, as shown in Fig. 4, and

262 2. averaging the highest 5% of the extracted rainfall rates.

263 Ultimately, the estimated maximum rainfall rates were searched for the
264 highest one, or momentary maximum rainfall rate, within 5 - 30 minutes
265 after the observation of peak column height (Section 3.1), whose time range
266 is based on lag correlations shown by Picca et al. (2010) and Kumjian et
267 al. (2014). The lag time between observations of peak column height and
268 momentary maximum rainfall rate near the ground was also calculated, as
269 depicted in Fig. 5.

Fig. 4

Fig. 5

270 **4. Relationship between peak Z_{DR} column height and** 271 **maximum rainfall rate**

272 Recent studies have demonstrated Z_{DR} column height to be closely asso-
273 ciated with updraft intensity; it increases before producing high reflectivity
274 at low levels (e.g., Kumjian et al. 2014, among others). To what extent,
275 therefore, is it correlated with the intensity of rainfall at ground level? To
276 address this remaining question, we explored the correlation between peak
277 Z_{DR} column height and momentary maximum rainfall rate near ground level
278 using the data acquired by dual-polarization radar.

279 On 11 July 2021, the Haneda radar observed tens of Z_{DR} columns as
280 columnar regions of enhanced Z_{DR} extending vertically above the estimated

281 0 °C level of 4.6 km AGL. Thirteen of these were selected as sample columns
282 in this study because they remained at sufficient distances from each other
283 to permit quantitative analysis. For each column, the maximum height in
284 the time evolution, or peak column height, was automatically calculated, as
285 described in Section 3.1. The maximum rainfall rate associated with each
286 column was then estimated using the current JMA algorithm of $R(K_{DP}, Z_H)$,
287 as detailed in Sections 3.2 and 3.3. Before conducting a regression analysis
288 between the peak column height and the maximum rainfall rate, we vali-
289 dated the radar rainfall estimates at the lowest elevation angle of 0.7° by
290 comparison with disdrometer measurements on the ground as follows.

291 *4.1 Validation of rainfall estimates*

292 Figure 6 displays the rainfall estimates from the Haneda radar compared
293 with those from the disdrometer installed at the Kumagaya observation site.
294 Here, the radar-derived rainfall rates are averaged within 1 - 2 km west
295 of the Kumagaya site on the basis of the environmental wind speed and
296 direction. Given that it takes a few minutes for raindrops to reach ground
297 level, the observation time of the disdrometer is adjusted by three minutes
298 to be equivalent to that of the radar. Although a few outliers are evident,
299 it can be seen in the figure that the radar-derived rainfall estimates agree
300 with the disdrometer measurements with a mean error of 15%.

Fig. 6

Fig. 7

301 Furthermore, we validated rainfall rates derived from the disdrometer by
302 comparison with rain gauge data, both taken from the Kumagaya observa-
303 tion site. Figure 7 shows that the 10-min averaged rainfall rates calculated
304 from the 1-min averaged disdrometer data agree quite well with those from
305 the rain gauge. Taken together with the comparison results shown in Fig.
306 6, this indicates that the rainfall rates derived from the radar data with a
307 temporal resolution of one minute agree with those observed on the ground.

308 4.2 Regression analysis

309 After the validation of radar rainfall estimates, we examined the corre-
310 lation between the peak Z_{DR} column height and the maximum rainfall rate
311 near ground level. The resultant correlations between the two are plotted
312 in Fig. 8, in which the horizontal and vertical axes respectively represent
313 the height above the 0 °C level and the maximum rainfall rate observed at
314 the lowest elevation angle of 0.7°.

Fig. 8

315 According to the regression analysis results, the regression line is repre-
316 sented as

$$y = 29.0x + 60.2, \quad (3)$$

317 where x is peak column height (km) and y is maximum rainfall rate (mm h^{-1})
318 near ground level. Although the correlation coefficient is not very high, at
319 0.64, this result indicates that a taller Z_{DR} column is likely linked to greater

320 production of rainfall. The figure also depicts lag times between observa-
321 tions of peak column height and maximum rainfall rate. About 60% of the
322 lag times for the thirteen columns were recorded within 8 - 12 minutes.

323 In Fig. 8, Column A has a relatively small residual in the linear regres-
324 sion and a normal lag time of 11.5 minutes among them. By contrast, a
325 data point in another sample column, called “Column B” hereinafter, devi-
326 ates considerably from the regression line, with the longest lag time of 24
327 minutes. In the following section, we discuss the evolution of both columns,
328 observed within the rectangular areas in Fig. 9, and the cause of the above
329 deviation.

Fig. 9

330 5. Discussion

331 5.1 *Evolution of Z_{DR} columns*

332 Recent studies have shown that a tall Z_{DR} column appears when a suffi-
333 ciently strong updraft lofts large raindrops well above the 0 °C level during
334 the development of convective clouds, and that as the column decays after
335 reaching a peak height, an area of high rainfall rates aloft descends to the
336 ground (e.g., Kumjian et al. 2014). Figures 10 and 11 both depict the time
337 evolution of Column A, beginning with the observation time of the peak
338 column height and ending with that of the maximum rainfall rate. The

339 3-dB Z_{DR} contour is superimposed over the field of Z_H , Z_{DR} , K_{DP} , and ρ_{HV}
 340 in Fig. 10, and over that of the highest rainfall rates within a 1km-wide
 341 range of the analyzed area in Fig. 11. The observation time at an elevation
 342 angle of 3.8° is shown in the upper left corner of each figure. Note that the
 343 cross-sections are reconstructed from several elevation-angle scans, thereby
 344 involving some degree of interpolation. In Fig. 10, the areas of high Z_H ,
 345 Z_{DR} , and K_{DP} with low ρ_{HV} at heights above the 0°C level suggest the
 346 presence of large raindrops lofted by strong updrafts. In Figs. 11a-c, the
 347 areas of maximum rainfall rates gradually descend to the ground as the col-
 348 umn decays. Figure 12 shows that the momentary maximum rainfall rate
 349 was observed 12 minutes after the column height reached a peak, at 15:14
 350 JST, using the data at the lowest elevation angle of 0.7° . Note that the
 351 time is about two minutes later than that shown in Fig. 11c because of the
 352 difference in the angles.

Fig. 10

Fig. 11

Fig. 12

Fig. 13

353 5.2 *Interference from hail*

354 Figure 13 depicts the time evolution of Column B, which has different
 355 characteristics from other columns (Fig. 8) and considerably high rainfall
 356 rates above the 0°C level, especially at 15:22 JST (Fig. 13c). The presence
 357 of hail is expected at these levels at sub-zero temperatures, which is not
 358 taken into account in the rainfall estimation algorithm (Section 3.2). For

359 this reason, the rainfall rates estimated for Column B are likely to be inac-
 360 curate. To confirm this inference, we examined the vertical distributions of
 361 K_{DP} , ρ_{HV} , and $R(K_{\text{DP}}, Z_{\text{H}})$ as in Fig. 14, modified from Fig. 13c. The areas
 362 of high K_{DP} overlap only slightly with those of $R(K_{\text{DP}}, Z_{\text{H}}) \geq 150 \text{ mm h}^{-1}$,
 363 denoted by the dashed contour, which reveals that the estimates of high
 364 rainfall rates are in error due to $R(Z_{\text{H}})$ being included in the measurement,
 365 caused by low K_{DP} and high Z_{H} . In other words, the mismatch of high K_{DP}
 366 and high $R(K_{\text{DP}}, Z_{\text{H}})$ implies incorrect radar rainfall estimation. Moreover,
 367 the areas of low ρ_{HV} superimposed with bold contours nearly overlap those
 368 of high $R(K_{\text{DP}}, Z_{\text{H}})$, which indicates that hail is present in those areas, since
 369 ρ_{HV} decreases in hail-mixed precipitation (Kumjian 2013a). The presence
 370 of hail is, therefore, likely to have caused the estimation error by increasing
 371 Z_{H} but leaving K_{DP} unaffected.

Fig. 14

372 5.3 *Improvement of rainfall estimation*

373 To reduce the effect of interference from hail, we recalculated low-level
 374 maximum rainfall rates after eliminating data with $R(K_{\text{DP}}, Z_{\text{H}}) > 1.5R(K_{\text{DP}})$
 375 and $R(K_{\text{DP}}, Z_{\text{H}}) > 100 \text{ mm h}^{-1}$ to detect heavy precipitation estimates that
 376 are strongly affected by the presence of hail. The recalculation led to an
 377 approximately 50% change in Column B but less than 15% for the other
 378 columns in the resultant maximum rainfall rates. Note that this algorithm

379 is applicable only to hail-mixed heavy rainfall estimation and does not work
380 for pure rain. The regression equation and the correlation coefficient be-
381 tween rainfall estimates from radar and disdrometer are

$$y = 1.14x + 0.95 \quad (R = 0.85), \quad (4)$$

382 where x is the rainfall rate derived from disdrometer (mm h^{-1}) and y is that
383 from radar (mm h^{-1}). They are approximately equal to those shown in Fig.
384 6b, which supports the validity of the algorithm.

385 Figure 15 shows the correlations between the peak Z_{DR} column height
386 and the maximum rainfall rate near ground level, where the recalculated
387 results for Columns A and B are denoted as Columns A' and B', respectively.
388 The equation of the regression line alters from Eq. (3) to

$$y = 20.7x + 75.6, \quad (5)$$

389 and the correlation coefficient changes to 0.61 because of the great reduc-
390 tion in the covariance between Z_{DR} column height and low-level maximum
391 rainfall rate.

Fig. 15

392 5.4 Forecast lead time

393 We explored lag times between observations of the peak column height
394 and the maximum rainfall rate as a function of peak column height, as
395 plotted in Fig. 16, where no correlation is shown, although enhanced Z_{DR}

396 suggests the presence of large raindrops. Instead, most of the lag times
397 were 9 - 12 minutes regardless of height, and the mean (standard error)
398 was 11.1 (± 1.06) minutes. Assuming that it takes several minutes for
399 raindrops to fall from the level of the lowest elevation measurement with
400 the radar to ground level, the expected forecast lead time is about 13 - 15
401 minutes, which precisely matches the peak lag correlation time arrived at
402 by numerical simulation in Kumjian et al. (2014). The figure also suggests
403 that convective clouds with Z_{DR} columns over 3 km tall have the potential
404 to produce extreme rainfall with an intensity of over 180 mm h^{-1} at ground
405 level.

Fig. 16

406 *5.5 Applicability of the quantitative relationship to other cases*

407 To validate the findings from the quantitative analysis on the thirteen
408 columns, we looked at nine Z_{DR} columns observed by the Haneda radar
409 above the estimated 0°C level of 5.9 km AGL on 12 August 2020, about 1
410 km higher than that on 11 July 2021. In Fig. 17, the peak column height
411 is positively correlated with the maximum rainfall rate near ground level,
412 and the correlation coefficient is 0.62.

Fig. 17

413 Figure 18 shows the correlation between the two, calculated using both
414 data collected on 11 July 2021 and 12 August 2020. The equation of the

415 regression line is

$$y = 26.3x + 51.8, \quad (6)$$

416 where x is peak column height (km) and y is maximum rainfall rate (mm h^{-1})
417 near ground level. The correlation coefficient is 0.68, the highest value in
418 this study. These results suggest that the quantitative relationship obtained
419 in this study is applicable to other rainfall events and that rainfall intensity
420 is likely to exceed 50 mm h^{-1} when radar identifies a Z_{DR} column over the
421 Kanto region in summer.

Fig. 18

422 The correlation between the peak column height and the lag time, cal-
423 culated using the data collected on 12 August 2020, is shown in Fig. 19,
424 in which those on 11 July 2021 are not plotted because of the difference in
425 the estimated $0 \text{ }^\circ\text{C}$ levels. According to the regression analysis results, the
426 regression line is represented as

$$y = 6.93x - 0.74, \quad (7)$$

427 where x is peak column height (km) and y is lag time (min). The fig-
428 ure shows a positive correlation with a coefficient of 0.68, which is likely
429 associated with the correlation between Z_{DR} column height and updraft in-
430 tensity. However, no correlation is shown in Fig. 16. Further analysis of
431 cases in various atmospheric conditions is needed to arrive at a definitive
432 understanding of the difference in correlations between them.

Fig. 19

433 6. Conclusions

434 The increasing use of dual-polarization radar in recent decades has al-
435 lowed progressive elucidation of the characteristics of Z_{DR} columns. For
436 example, growth in the volume of a Z_{DR} column appears before an increase
437 in radar reflectivity at low levels (e.g., Picca et al. 2010). The location and
438 height of a Z_{DR} column are closely related to the position and intensity of
439 updrafts, respectively (e.g., Snyder et al. 2015). Although Z_{DR} columns are
440 increasingly regarded as a predictive tool for extreme rainfall, it remains
441 unclear how well they are associated with rainfall intensity on the ground
442 and to what extent they can be applied to weather prediction.

443 Our quantitative research using dual-polarization radar measurements
444 reveals a positive correlation between peak Z_{DR} column height and maxi-
445 mum rainfall rate near ground level, indicating that Z_{DR} columns should
446 be able to provide useful information on expected rainfall intensity. For in-
447 stance, when radar identifies a Z_{DR} column, rainfall intensity on the ground
448 is likely to exceed 50 mm h^{-1} and continue to increase while the column
449 grows in height. A column over 3 km tall from the environmental $0 \text{ }^\circ\text{C}$ level
450 can be a precursor of extreme rainfall with an intensity of 180 mm h^{-1} or
451 more. The heaviest rainfall is likely to occur about 10 - 20 minutes after
452 a Z_{DR} column matures, though more studies are required to determine the
453 definitive forecast lead time. Our findings suggest that Z_{DR} column mea-

454 surement can help to improve very short-range forecasts and/or nowcasts
455 and lead to early warnings and better disaster management of localized
456 rainfall extremes and the damaging floods that result from them.

457 On the other hand, the resultant correlation might be improved by ap-
458 plying additional meteorological data or environmental factors. As an ex-
459 ample, certain convective parameters, such as convective available potential
460 energy (CAPE), may strengthen the correlation if integrated into the data
461 analysis. Additionally, with further studies on Z_{DR} columns, a better un-
462 derstanding of cloud microphysical processes in convective clouds might,
463 for instance, contribute to the development of numerical weather predic-
464 tion models through the identification of updraft regions. In brief, more
465 advanced research is needed in future to enhance the effectiveness of oper-
466 ational applications of Z_{DR} columns for severe weather prediction.

467 Appendix

468 Disdrometer measurements

469 The Parsivel disdrometer records rainfall rates derived from its onboard
470 ASDO software, but they tend to be overestimated during heavy rainfall
471 events (Thurai et al. 2011). Adachi et al. (2013) suggest that this ten-
472 dency is likely to occur because the diameters determined by Parsivel¹ are

473 not volume-equivalent: they are only the maximum horizontal diameters
474 of particles. For this reason, we recalculated rainfall rates using DSD data
475 obtained through converting horizontal diameters of raindrops into volume-
476 equivalent versions on the basis of the model axis ratio presented by Beard
477 and Chuang (1987) and reducing the influence of strong wind and turbu-
478 lence as proposed by Friedrich et al. (2013). The equation for calculating
479 rainfall rates is expressed as

$$R = 6 \times 10^{-4} \pi \sum_{p=1}^{32} \frac{C_p D_p^3}{S \cdot \Delta t}, \quad (8)$$

480 where R is rainfall rate (mm h^{-1}), C_p and D_p are the number and the
481 volume equivalent diameter (mm) of the particles in the 32 size classes, S
482 is the measuring area (m^2), and Δt is the sampling time (s).

483 Data Availability Statement

484 The observational data from radar and disdrometer measurements ana-
485 lyzed in this study, which respectively belong to the Japan Meteorological
486 Agency (JMA) and Meteorological Research Institute (MRI), are available
487 from the corresponding author upon reasonable request. The precipitation
488 data from the rain gauge is available at [https://www.data.jma.go.jp/](https://www.data.jma.go.jp/gmd/risk/obsdl/index.php)
489 [gmd/risk/obsdl/index.php](https://www.data.jma.go.jp/gmd/risk/obsdl/index.php) (in Japanese).

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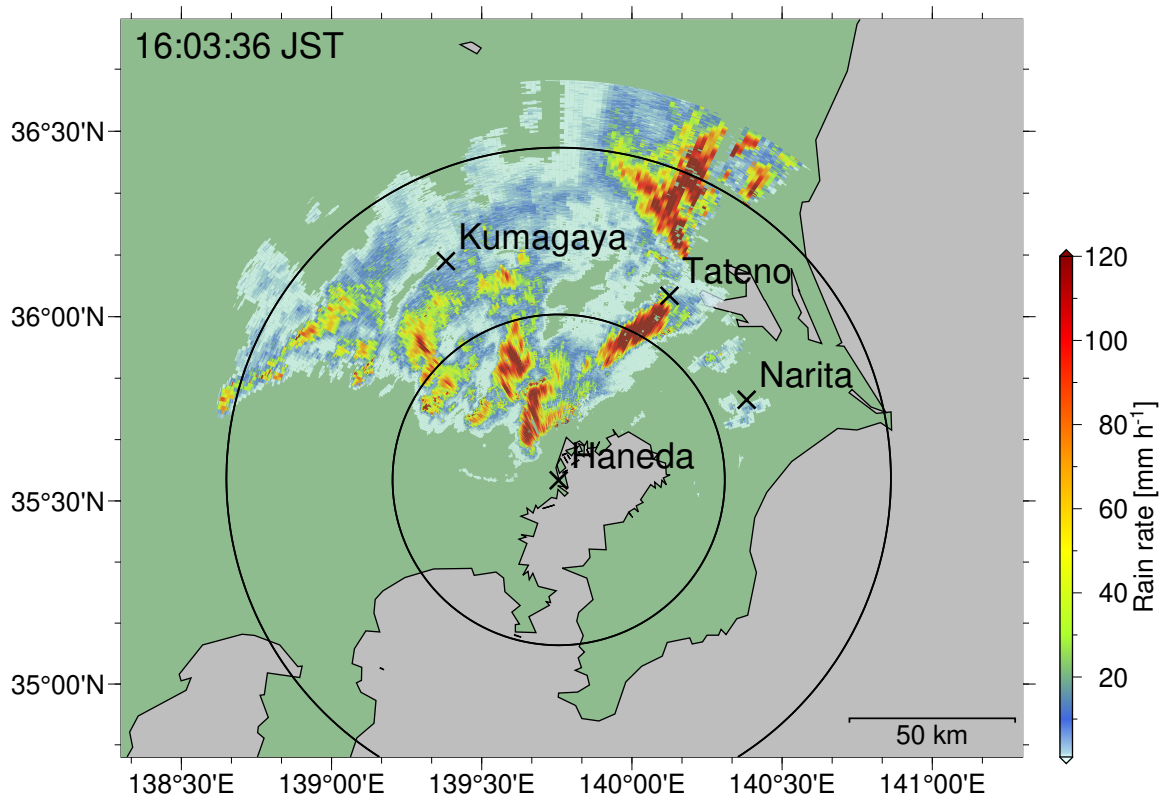


Fig. 1: A snapshot of the estimated rain field from a PPI scan at 1.1° elevation angle performed by the Haneda radar at 16:03 JST on 11 July 2021. Black crosses denote the locations of the Haneda and Narita radar, and the Kumagaya and Tateno observation sites. The two black circles indicate 50-km and 100-km distances from the Haneda radar.

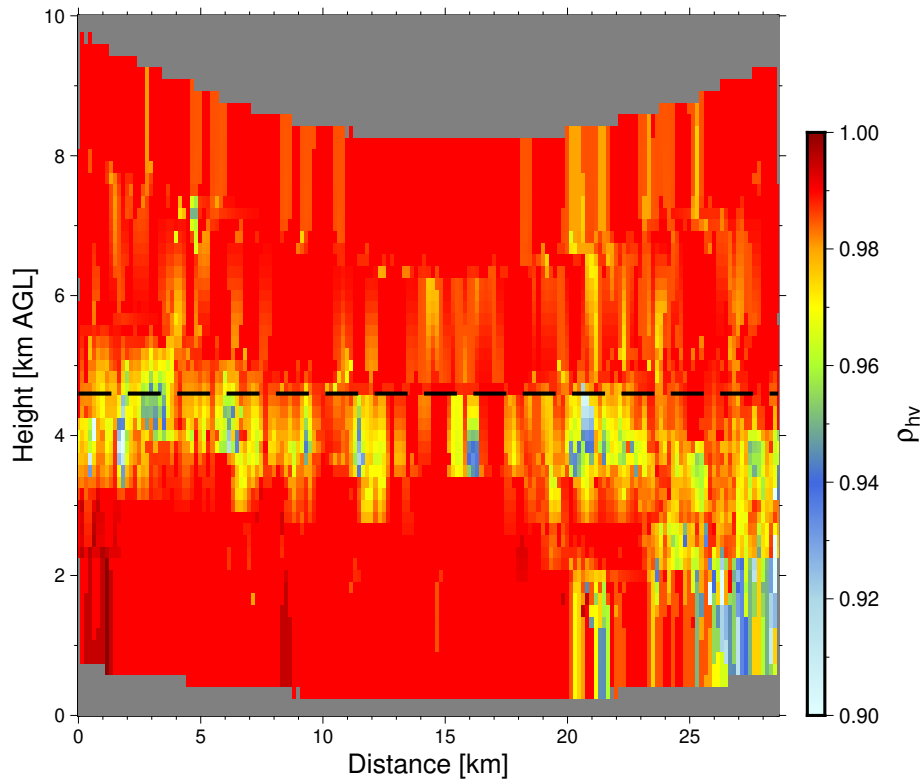


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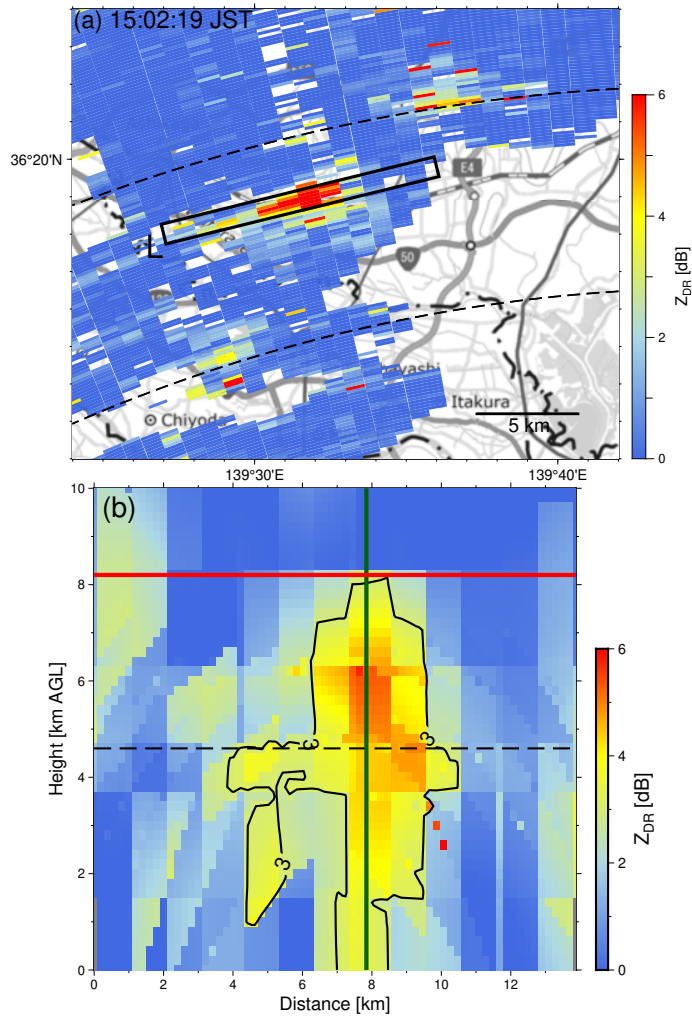


Fig. 3: Snapshots of a sample column

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(b) Vertical distribution of Z_{DR} overlaid with lines indicating estimated height (red), central axis (green), estimated 0°C level of 4.6 km AGL (dashed black), and 3-dB Z_{DR} contour (solid black). The horizontal axis represents the distance from the west end of the rectangle, denoted by letter “L” in (a).

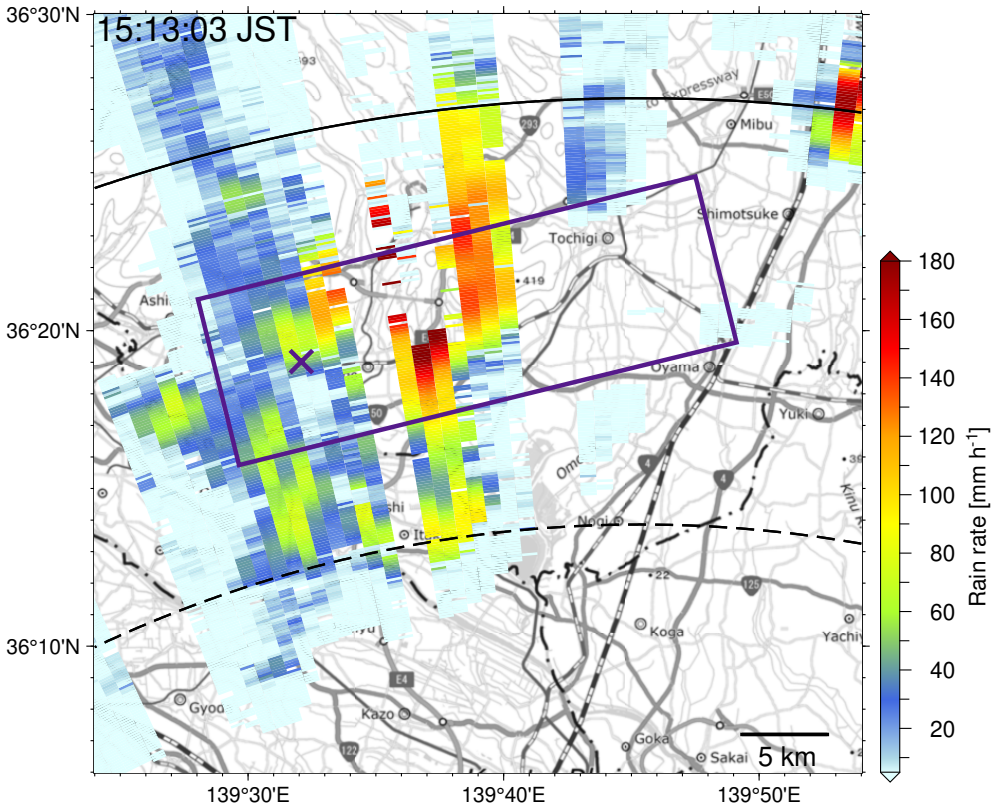


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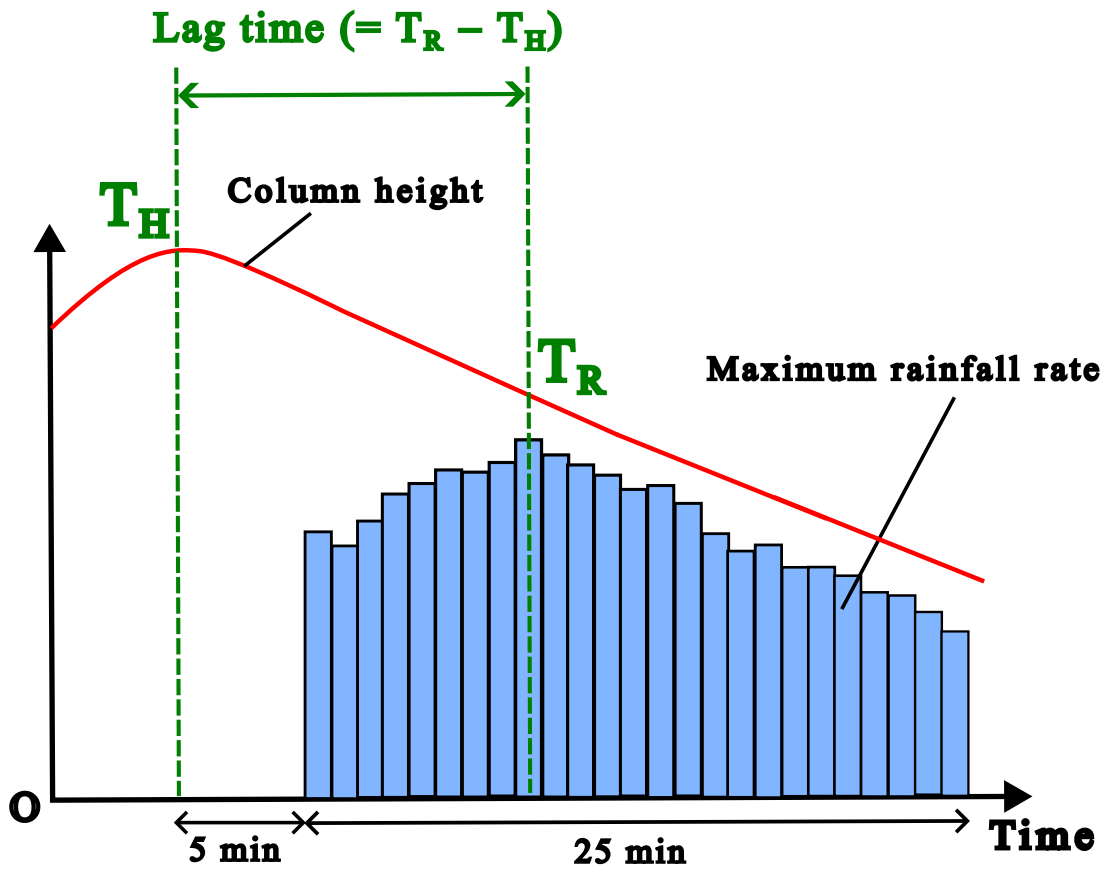


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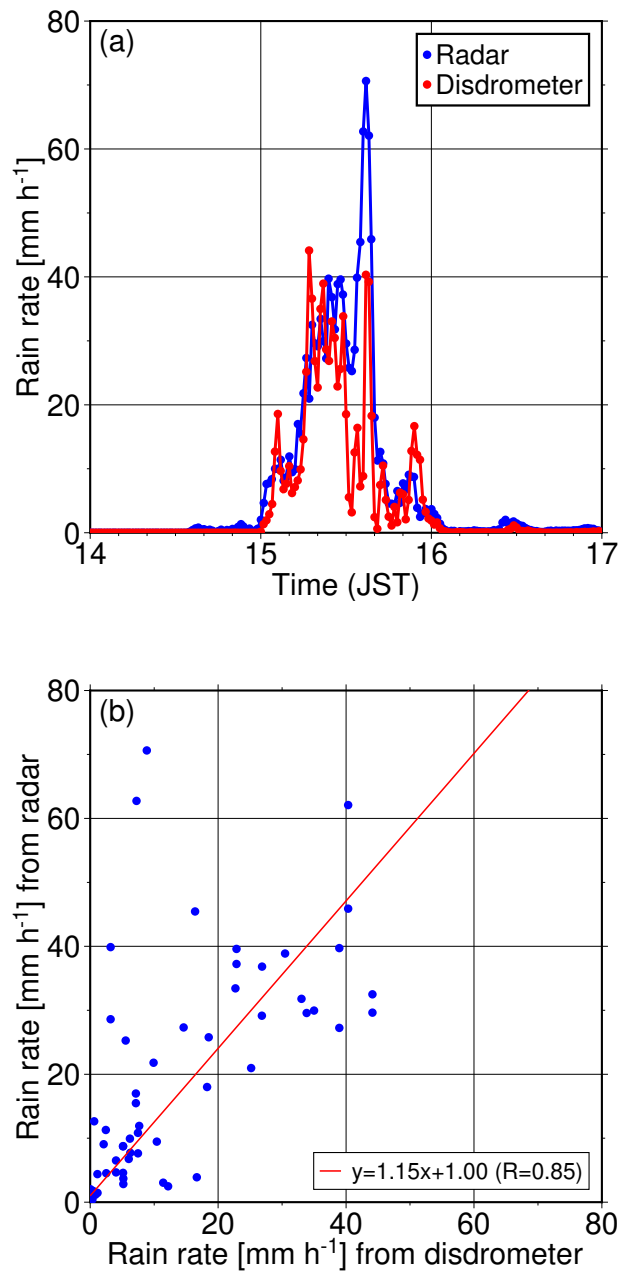


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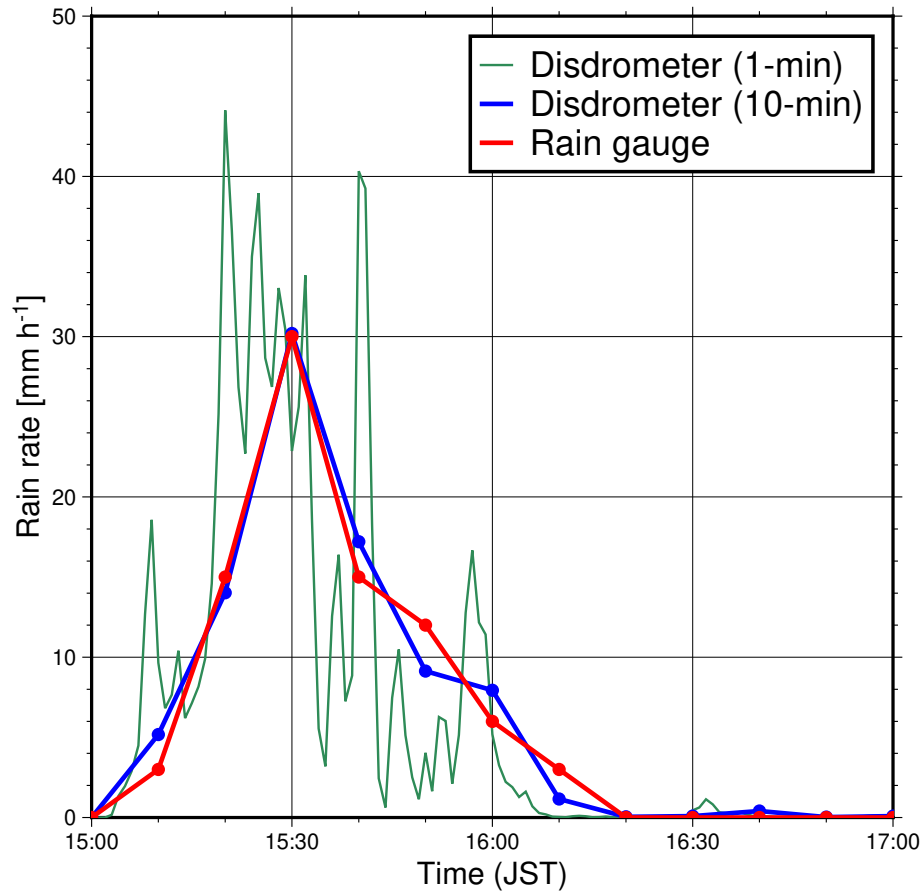


Fig. 7: Time series of rainfall rates from the disdrometer (1-min average in green, 10-min average in blue) and the rain gauge (red) at the Kumagaya site, observed on 11 July 2021.

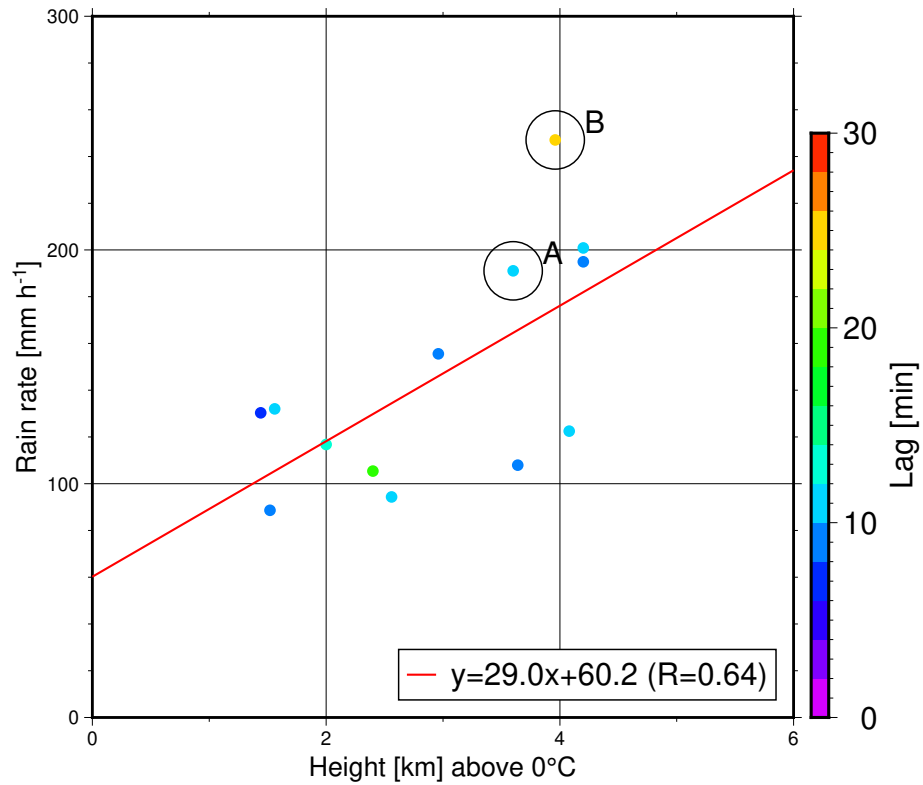


Fig. 8: Scatter plots of peak Z_{DR} column height above the 0 °C level vs. the maximum rainfall rate at low levels, observed on 11 July 2021, with the color scale representing the lag time between observations. Black circles denote the data for Columns A and B, and the red line shows the linear regression. The regression equation and the correlation coefficient are shown in the lower right corner.

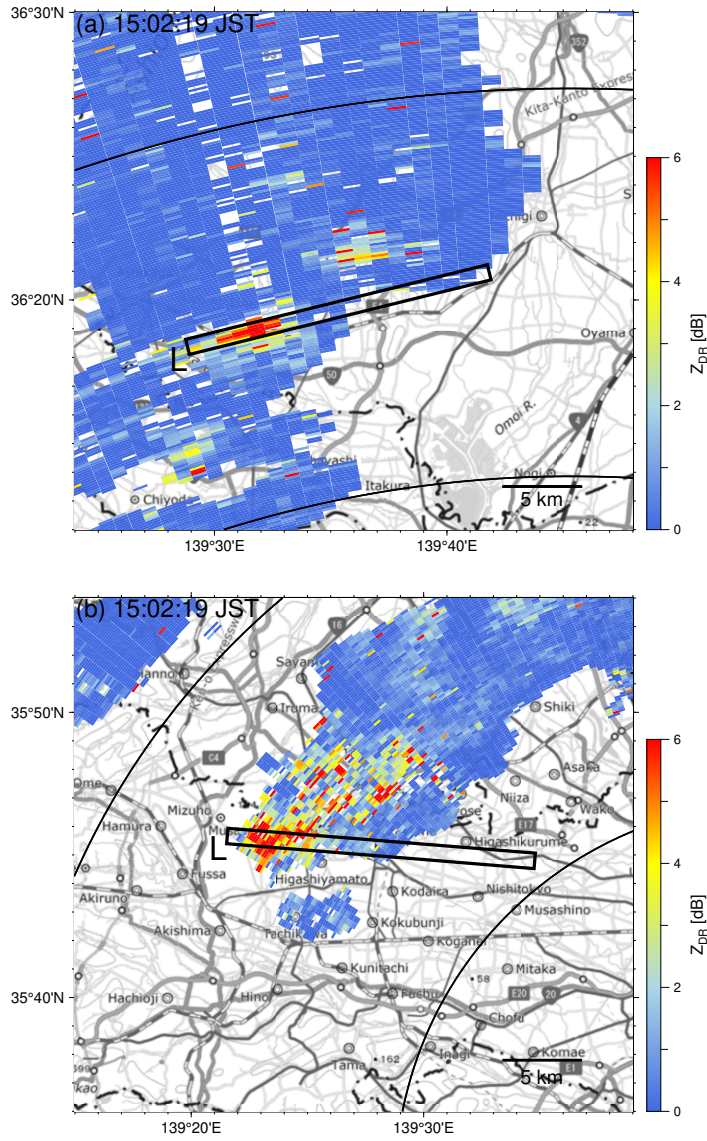


Fig. 9: PPI scan of Z_{DR} at 3.8° elevation angle performed by the Haneda radar at 15:02 JST on 11 July 2021. The base map was obtained from the GSI.

(a) A snapshot of Column A. Black arcs indicate 50-km and 100-km distances from the radar. Black rectangle (1×20 km) and letter “L” respectively denote the analyzed area and the starting point to count the horizontal distance in Figs. 10 and 11.

(b) A snapshot of Column B. Black arcs indicate 150-km and 200-km distances from the radar. Black rectangle (1×20 km) and letter “L” respectively denote the analyzed area and the starting point to count the horizontal distance in Fig. 13.

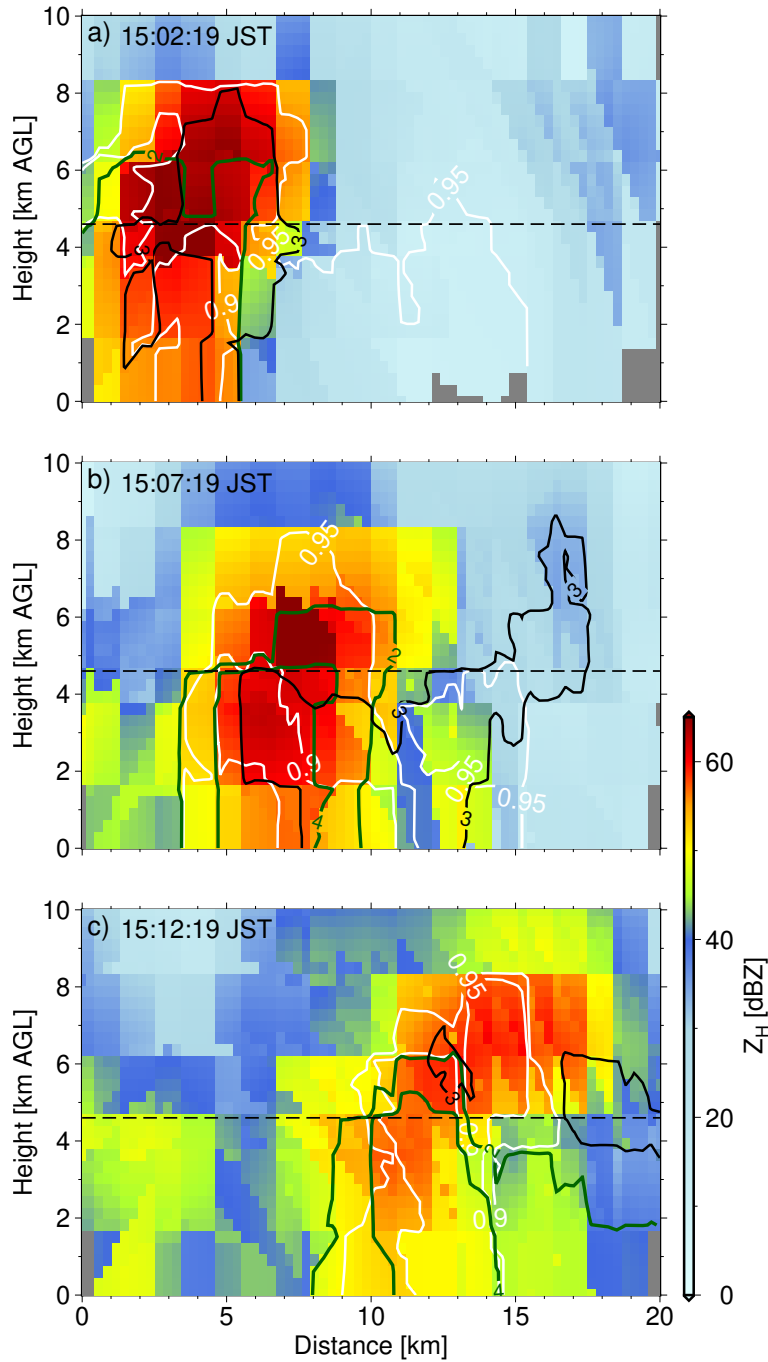


Fig. 10: Vertical distributions of Z_H overlaid with a Z_{DR} contour of 3 dB (solid black), K_{DP} contours of 2 and 4 deg/km (solid green), ρ_{HV} contours of 0.9 and 0.95 (solid white), the environmental 0 °C level of 4.6 km AGL (dashed black), and the observation time at 3.8° elevation angle in the upper left corner, representing the evolution of Column A. The horizontal axis represents the distance from the point denoted by the letter “L” in Fig. 9a. Note that Column A is the lower one with a height of 4.6 km AGL in (b).

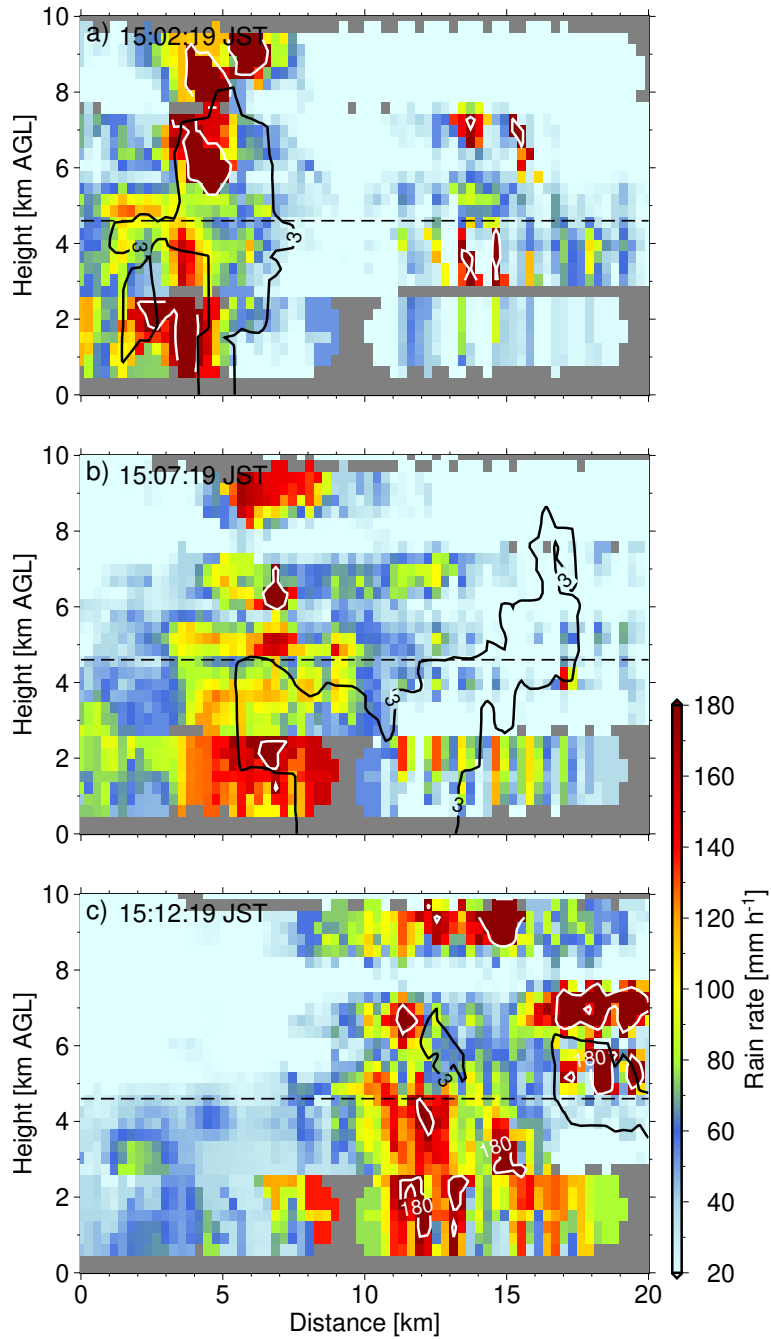


Fig. 11: As in Fig. 10, but the color scale represents the highest $R(K_{DP}, Z_H)$ within a 1km-wide range of the area indicated in Fig. 9a, with the contour of 180 mm h^{-1} (solid white).

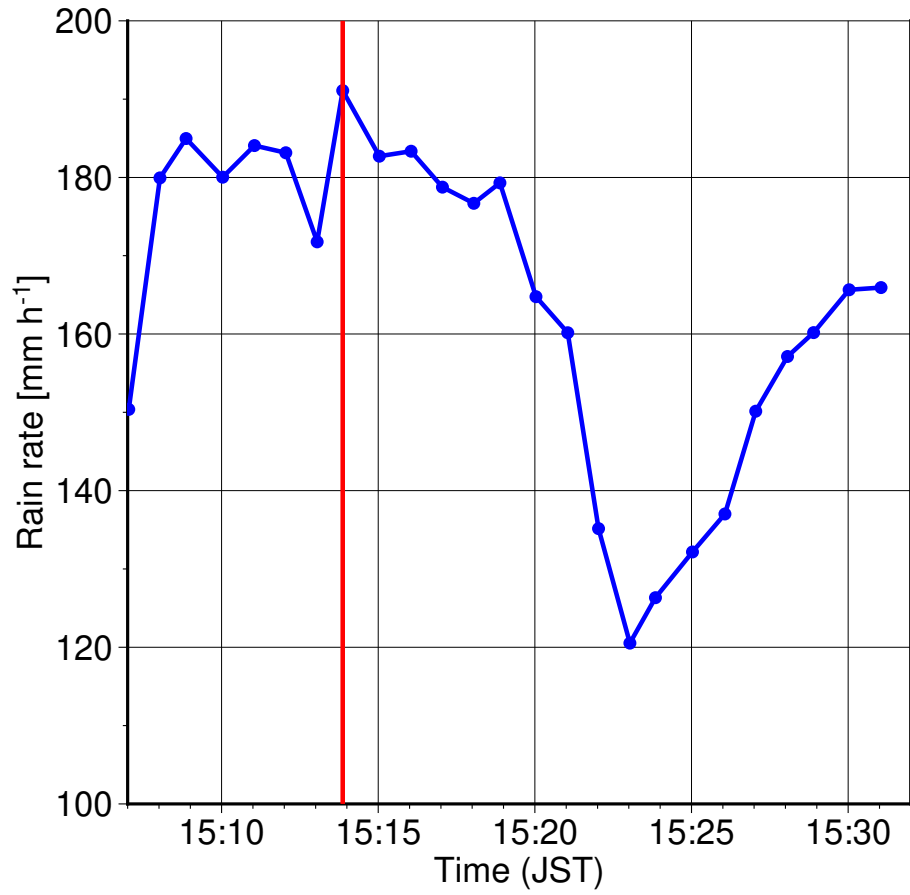


Fig. 12: Time series of the maximum rainfall rates within 5 - 30 minutes after the observation of the peak height of Column A observed at 15:02 JST at 0.7° elevation angle. The red line indicates the observation time of the momentary maximum rainfall rate.

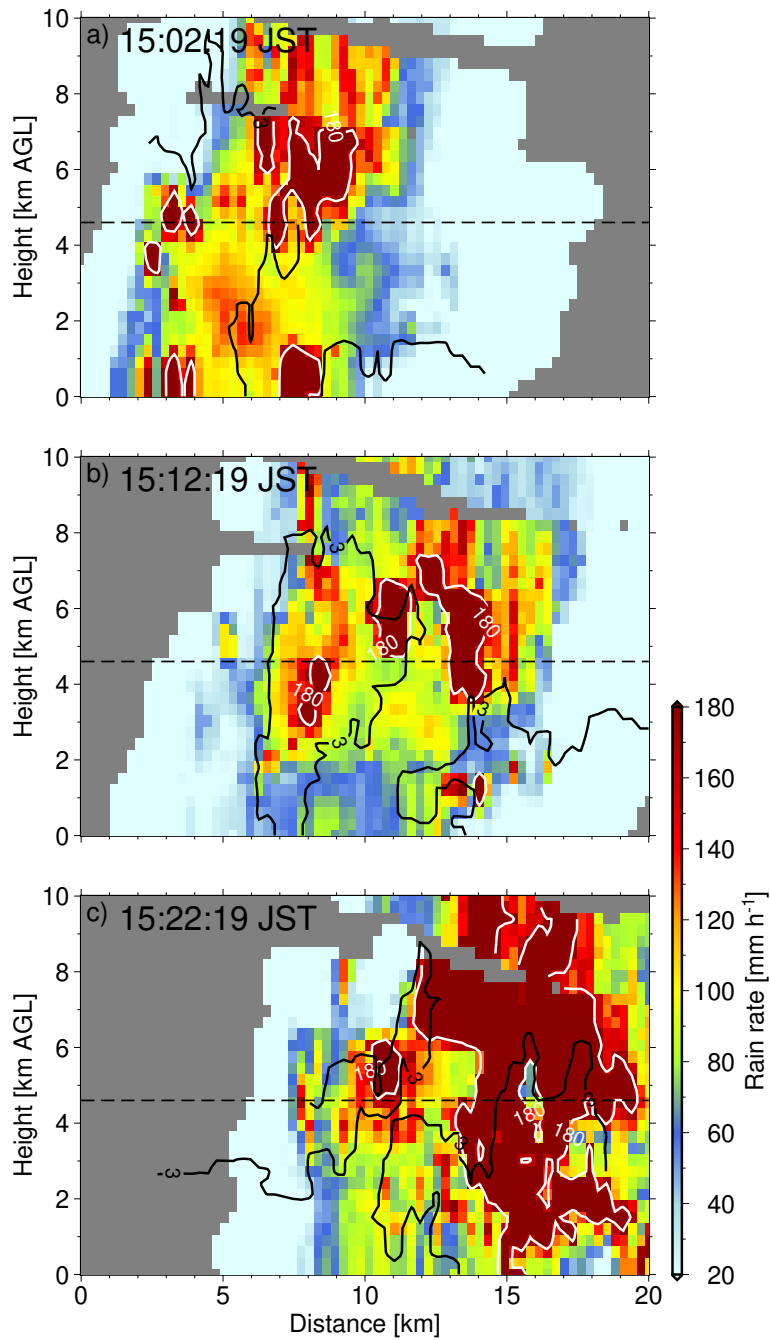


Fig. 13: As in Fig. 11, but the evolution of Column B is represented. The horizontal axis indicates the distance from the point denoted by the letter “L” in Fig. 9b.

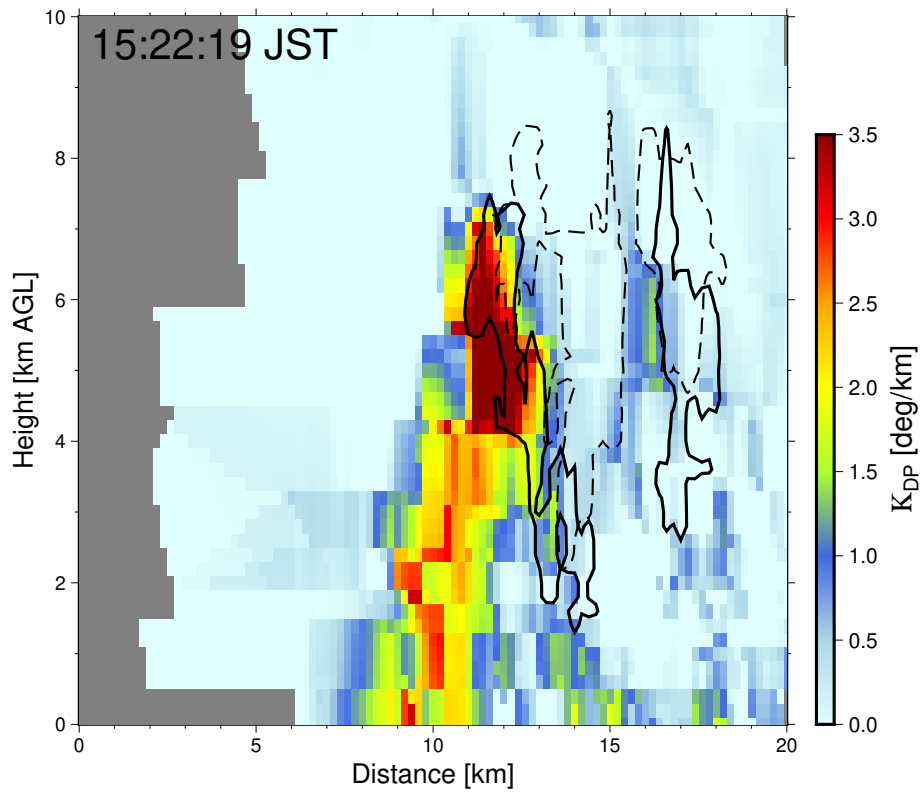


Fig. 14: Vertical distribution of K_{DP} calculated for Column B, overlaid with a ρ_{HV} contour of 0.86 (bold black), $R(K_{DP}, Z_H)$ contour of 150 mm h⁻¹ (dashed black), and the observation time in the upper left corner.

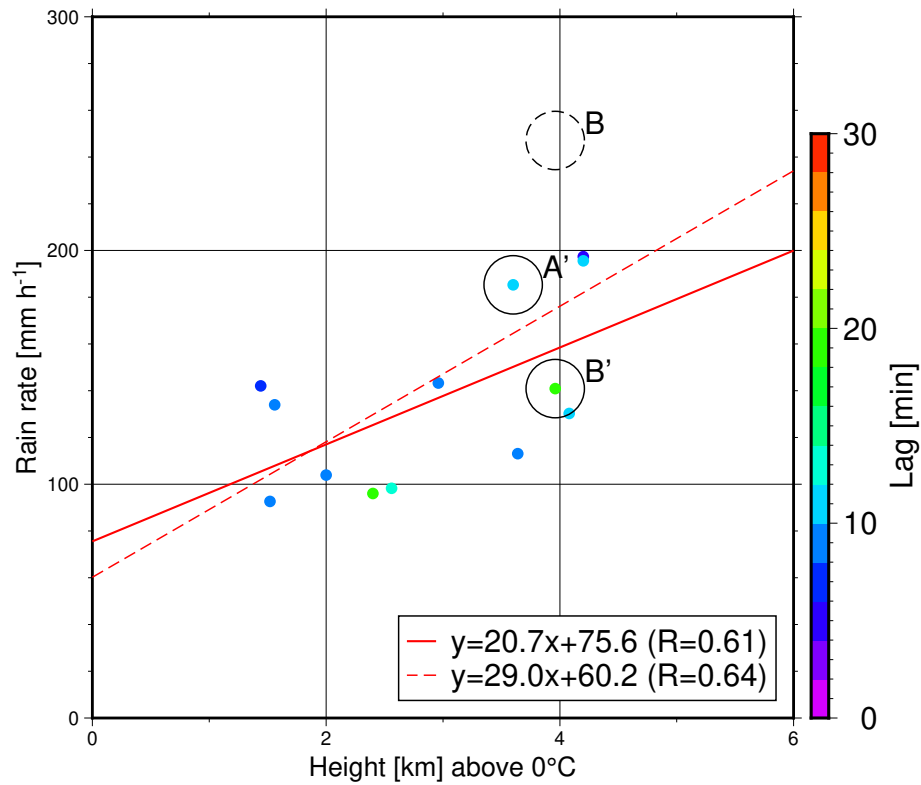


Fig. 15: As in Fig. 8, but the data are recalculated after eliminating those affected by hail. Solid black circles denote the data for Columns A' and B'. For reference, the dashed black circle denotes the original data for Column B, and the dashed red line shows the linear regression before recalculation.

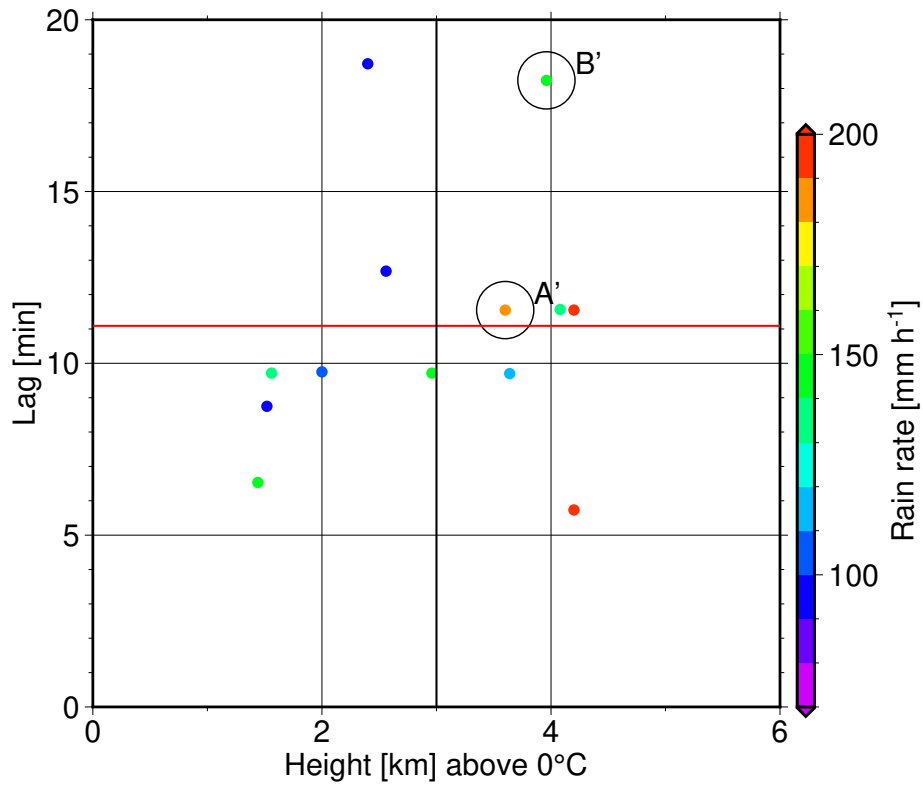


Fig. 16: Scatter plots of peak Z_{DR} column height above 0 °C level vs. lag time between peak column height and maximum rainfall rate observations, with the color scale representing maximum rainfall rates. Black and red lines respectively indicate 3 km height and mean lag time (11.1 min), and solid black circles denote the data for Columns A' and B'.

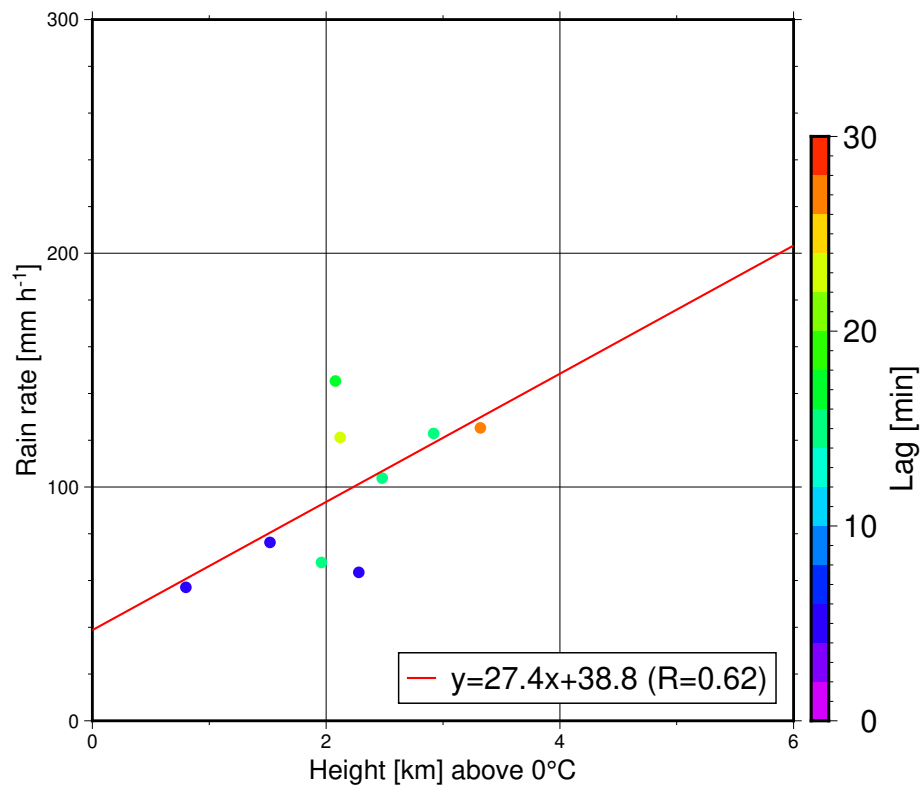


Fig. 17: As in Fig. 8, but the data were observed on 12 August 2020.

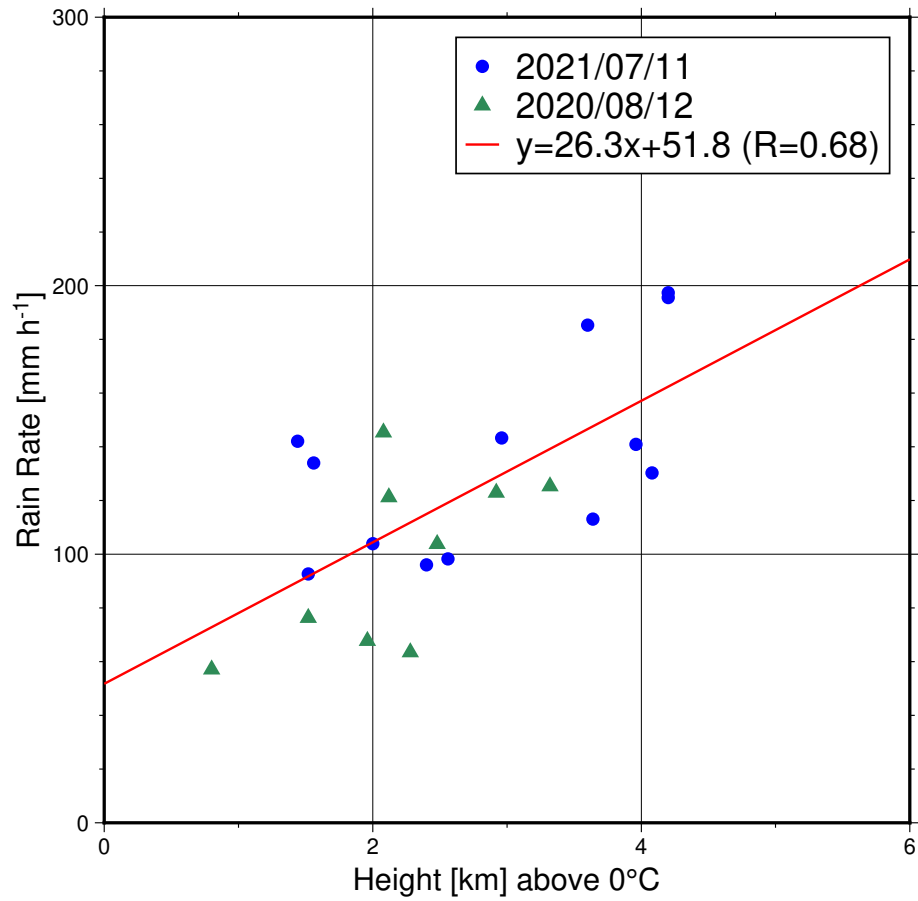


Fig. 18: Scatter plots of peak Z_{DR} column height above the 0 °C level vs. the maximum rainfall rate at low levels. Blue circular and green triangular dots respectively represent the data collected on 11 July 2021 and those on 12 August 2020. The red line shows the linear regression, and the regression equation and the correlation coefficient are shown in the upper right corner.

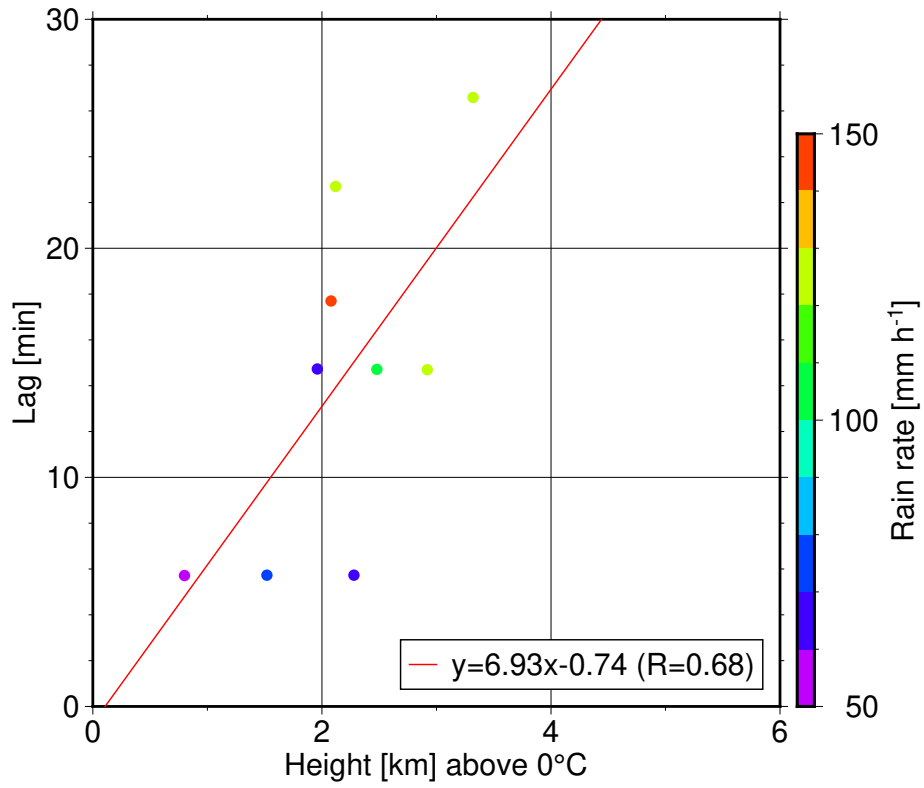


Fig. 19: As in Fig. 16, but the data were observed on 12 August 2020. The red line shows the linear regression, and the regression equation and the correlation coefficient are shown in the lower right corner.

List of Tables

733 1 Operating characteristics of the Haneda radar 57

Table 1: Operating characteristics of the Haneda radar

Frequency	5330 MHz
Peak power	5 kW
Pulse length	1 μ s (short pulse) 64 μ s (long pulse)
Antenna diameter	7.0 m
Antenna speed	4.2 rpm, 5.4 rpm, 7.0 rpm
Antenna gain (H and V)	> 49 dBi
Signal minimum	< -115 dBm
Cross-polar isolation	< -35 dB
Beam width	0.58° (horizontal) 0.59° (vertical)
Azimuthal resolution	0.7°
Transmitter	GaN HEMT
Range resolution	150 m
PRF	1040/832 Hz ($0.7^\circ \leq \text{Elv.} \leq 9.2^\circ$) 1365/1092 Hz (Elv. = 12.5°, 17.0°, 90°)